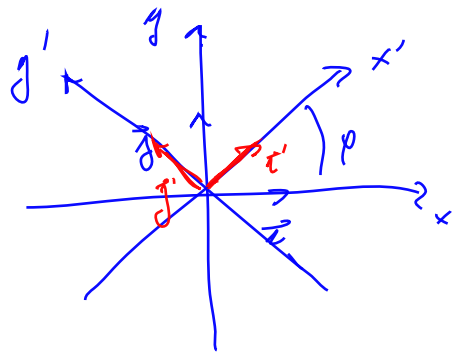


- Ravninsko napetostno stanje.

$$\underline{\underline{\boldsymbol{\epsilon}}} = \begin{bmatrix} \epsilon_{11} & \epsilon_{12} & 0 \\ \epsilon_{12} & \epsilon_{22} & 0 \\ 0 & 0 & 0 \end{bmatrix}$$



Komponentni zapis tenzorja napetosti.

$$\underline{\hat{i}}' = \cos\varphi \underline{\hat{i}} + \sin\varphi \underline{\hat{j}}$$

$$\underline{\hat{j}}' = -\sin\varphi \underline{\hat{i}} + \cos\varphi \underline{\hat{j}}$$

$$|\underline{\hat{i}}'| = 1, |\underline{\hat{j}}'| = 1, \underline{\hat{i}}' \cdot \underline{\hat{j}}' = 0$$

$$\underline{\underline{\underline{T}}} = \begin{bmatrix} t_{11} & t_{12} \\ t_{12} & t_{22} \end{bmatrix}$$

$$\underline{\underline{\underline{T}}} \cdot \underline{\hat{i}} = \begin{bmatrix} t_{11} & t_{12} \\ t_{12} & t_{22} \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix} = \begin{bmatrix} t_{11} \\ t_{12} \end{bmatrix}$$

$$\underline{\hat{i}} \cdot \underline{\underline{\underline{T}}} \underline{\hat{i}} = \begin{bmatrix} 1 \\ 0 \end{bmatrix} \cdot \begin{bmatrix} t_{11} \\ t_{12} \end{bmatrix} = t_{11}$$

$$t_{12} = \underline{\hat{i}} \cdot \underline{\underline{\underline{T}}} \underline{\hat{j}}; \quad t_{22} = \underline{\hat{j}} \cdot \underline{\underline{\underline{T}}} \underline{\hat{j}}$$

$$t_{11}' = \underline{\hat{i}}' \cdot \underline{\underline{\underline{T}}} \underline{\hat{i}}' = \begin{bmatrix} \cos\varphi \\ \sin\varphi \end{bmatrix} \cdot \begin{bmatrix} t_{11} & t_{12} \\ t_{12} & t_{22} \end{bmatrix} \begin{bmatrix} \cos\varphi \\ \sin\varphi \end{bmatrix} =$$

Ravnovesna enačba

$$= \begin{bmatrix} \cos\varphi \\ \sin\varphi \end{bmatrix} \cdot \begin{bmatrix} t_{11} \cos\varphi + t_{12} \sin\varphi \\ t_{12} \cos\varphi + t_{22} \sin\varphi \end{bmatrix} =$$

$$= t_{11} \cos^2\varphi + t_{12} \cos\varphi \sin\varphi + t_{12} \sin\varphi \cos\varphi + t_{22} \sin^2\varphi =$$

$$\cos^2\varphi = \frac{1}{2}(1 + \cos 2\varphi)$$

$$\sin^2\varphi = \frac{1}{2}(1 - \cos 2\varphi)$$

$$t_{11}' = \frac{1}{2}(t_{11} + t_{22}) + \frac{1}{2}(t_{11} - t_{22}) \cos 2\varphi + t_{12} \sin 2\varphi$$

$$t_{22}' = \underline{\hat{j}}' \cdot \underline{\underline{\underline{T}}} \underline{\hat{j}}' = \begin{bmatrix} -\sin\varphi \\ \cos\varphi \end{bmatrix} \cdot \begin{bmatrix} t_{11} & t_{12} \\ t_{12} & t_{22} \end{bmatrix} \begin{bmatrix} -\sin\varphi \\ \cos\varphi \end{bmatrix} =$$

$$= \begin{bmatrix} -\sin\varphi \\ \cos\varphi \end{bmatrix} \begin{bmatrix} -t_{11} \sin\varphi + t_{12} \cos\varphi \\ -t_{12} \sin\varphi + t_{22} \cos\varphi \end{bmatrix} =$$

$$= t_{11} \sin^2\varphi - t_{12} \sin\varphi \cos\varphi - t_{12} \cos\varphi \sin\varphi + t_{22} \cos^2\varphi =$$

$$t_{22}' = \frac{1}{2}(t_{11} + t_{22}) + \frac{1}{2}(-t_{11} + t_{22}) \cos 2\varphi - t_{12} \sin 2\varphi - \frac{1}{2}(t_{11} - t_{22}) \cos 2\varphi$$

Ravninsko napetostno stanje

Odvisnost komponent napetostnega tenzorja od postavitve koordinatnega sistema.

$$\begin{aligned} \tau'_{12} &= \bar{n}' \cdot \underline{\underline{\tau}} \cdot \bar{g}' = \begin{bmatrix} \cos \varphi \\ \sin \varphi \end{bmatrix} \cdot \begin{bmatrix} \tau_{11} & \tau_{12} \\ \tau_{12} & \tau_{22} \end{bmatrix} \begin{bmatrix} -\sin \varphi \\ \cos \varphi \end{bmatrix} = \\ &= \begin{bmatrix} \cos \varphi \\ \sin \varphi \end{bmatrix} \begin{bmatrix} -\tau_{11} \sin \varphi + \tau_{12} \cos \varphi \\ -\tau_{12} \sin \varphi + \tau_{22} \cos \varphi \end{bmatrix} = \\ &= -\tau_{11} \cos \varphi \sin \varphi + \tau_{12} \cos^2 \varphi - \tau_{12} \sin^2 \varphi + \tau_{22} \sin \varphi \cos \varphi = \\ \tau'_{12} &= -\frac{1}{2} (\tau_{11} - \tau_{22}) \sin 2\varphi + \tau_{12} \cos 2\varphi \end{aligned}$$

Ravninska mreža

$$\frac{d}{dx} (A\sigma) + p(x) = 0$$

$$\operatorname{div} \underline{\underline{\tau}} + \vec{f} = \vec{0}$$

\vec{f} volumenska gostota sil
 $\vec{p}\vec{g}$ je volumenska gostota
 sil teže.

$$\operatorname{div} \underline{\underline{\tau}} = \begin{bmatrix} \frac{\partial \tau_{11}}{\partial x} + \frac{\partial \tau_{12}}{\partial y} + \frac{\partial \tau_{13}}{\partial z} \\ \frac{\partial \tau_{12}}{\partial x} + \frac{\partial \tau_{22}}{\partial y} + \frac{\partial \tau_{23}}{\partial z} \\ \frac{\partial \tau_{13}}{\partial x} + \frac{\partial \tau_{23}}{\partial y} + \frac{\partial \tau_{33}}{\partial z} \end{bmatrix}$$

$$\frac{\partial}{\partial x} (x^2 y^2) = 2xy^2$$

$$\frac{\partial}{\partial y} (x^2 y^3) = 3x^2 y^2$$

$$\underline{\underline{\tau}} = \begin{bmatrix} \sigma & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$\operatorname{div} \underline{\underline{\tau}} = \begin{bmatrix} \frac{\partial \sigma}{\partial x} \\ 0 \\ 0 \end{bmatrix}$$

$$\frac{\partial \sigma}{\partial x} \vec{e}_1 + \vec{f} = \vec{0}$$

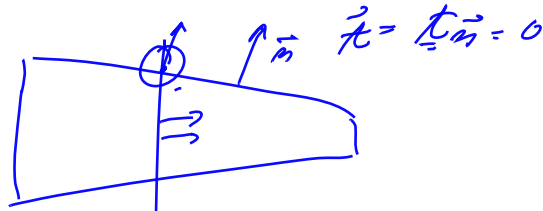
$$\vec{f} = f \vec{e}_1 ;$$

$$\left[\frac{\partial \sigma}{\partial x} + f = 0 \right] \quad f = \rho g \quad \frac{d}{dx} (A\sigma) + p = 0$$

$$\frac{d}{dx} (A\sigma) + fA = 0 \quad p = f \cdot A$$

V koordinatnem sistemu z osema $\vec{i}' = \cos \varphi \vec{i} + \sin \varphi \vec{j}$ in $\vec{j}' = -\sin \varphi \vec{i} + \cos \varphi \vec{j}$ je

$$\left(\begin{array}{l} \rightarrow \\ \rightarrow \\ \rightarrow \end{array} \right. \begin{array}{l} t'_{11} = \frac{1}{2}(t_{11} + t_{22}) + \frac{1}{2}(t_{11} - t_{22}) \cos 2\varphi + t_{12} \sin 2\varphi, \\ t'_{22} = \frac{1}{2}(t_{11} + t_{22}) - \frac{1}{2}(t_{11} - t_{22}) \cos 2\varphi - t_{12} \sin 2\varphi, \\ t'_{12} = -\frac{1}{2}(t_{11} - t_{22}) \sin 2\varphi + t_{12} \cos 2\varphi. \end{array} \left. \right)$$



$$Sl \underline{t} = t_{11} + t_{22} = t'_{11} + t'_{22} \quad \checkmark$$

$$t_{11} t_{22} - t_{12}^2 = t'_{11} t'_{22} - t_{12}'^2$$

$$t'_{11} = a + b$$

$$t'_{22} = a - b$$

$$t'_{11} t'_{22} - t_{12}'^2 = \left(\frac{1}{2}(t_{11} + t_{22}) \right)^2 - \left(\frac{1}{2}(t_{11} - t_{22}) \cos 2\varphi + t_{12} \sin 2\varphi \right)^2 - \left(-\frac{1}{2}(t_{11} - t_{22}) \sin 2\varphi + t_{12} \cos 2\varphi \right)^2 =$$

$$= \left(\frac{1}{2}(t_{11} + t_{22}) \right)^2 - \left(\left(\frac{1}{2}(t_{11} - t_{22}) \right)^2 + t_{12}^2 \right) = \frac{1}{4} (t_{11}^2 + t_{22}^2 + 2t_{11}t_{22}) - \frac{1}{4} (t_{11}^2 + t_{22}^2 - 2t_{11}t_{22}) - t_{12}^2 =$$

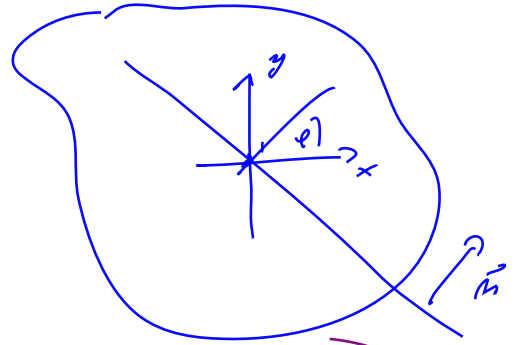
Invariante napetostnega tenzorja sta:

- sled napetostnega tenzorja (vsota diagonalnih elementov)
- determinanta napetostnega tenzorja

$$= \frac{1}{4} (t_{11}^2 + t_{22}^2 + 2t_{11}t_{22}) - \frac{1}{4} (t_{11}^2 + t_{22}^2 - 2t_{11}t_{22}) - t_{12}^2 = t_{11}t_{22} - t_{12}^2$$

Ekstremalne lastnosti napetostnega tenzorja

Določitev smeri ekstremalne normalne napetosti



$$\sigma_n = \sigma = \sigma_{n1} = \frac{1}{2}(t_{11} + t_{22}) + \frac{1}{2}(t_{11} - t_{22}) \cos 2\varphi + t_{12} \sin 2\varphi$$

$$A \cos 2\varphi + B \sin 2\varphi = \quad A = \frac{1}{2}(t_{11} - t_{22}); \quad B = t_{12}$$

$$= C \cos(2\varphi - \delta) = C \cos 2\varphi \cos \delta + C \sin 2\varphi \sin \delta$$

$$\boxed{A = C \cos \delta} \quad B = C \sin \delta \quad A^2 + B^2 = C^2 \Rightarrow C = \pm \sqrt{A^2 + B^2}$$

$$A \neq 0 \quad \frac{B}{A} = \frac{C \sin \delta}{C \cos \delta} = \tan \delta \Rightarrow \delta = \arctan \frac{B}{A} + k\pi; \quad \delta \in (-\pi/2, \pi/2)$$

$$\text{Izberimo } C > 0; \quad A > 0; \quad \checkmark$$

$$A < 0; \quad \cos(\delta + \pi) = -\cos \delta$$

$$\delta \in (\pi/2, 3\pi/2) \quad \checkmark$$

$$\sigma_{n1} = \frac{1}{2}(t_{11} + t_{22}) + \sqrt{A^2 + B^2} \cos(2\varphi - \delta) \quad \delta \in (-\pi/2, \pi/2) \quad A > 0$$

$$\delta \in (\pi/2, 3\pi/2) \quad A < 0$$

$$\sigma_{\text{akt}} = \frac{1}{2}(t_{11} + t_{22}) \pm \sqrt{\left(\frac{1}{2}(t_{11} - t_{22})\right)^2 + t_{12}^2} = \frac{1}{2} \left(t_{11} + t_{22} \pm \sqrt{(t_{11} - t_{22})^2 + 4t_{12}^2} \right)$$

$$2\varphi - \delta = 0 \quad \text{max}; \quad 2\varphi - \delta = \pi \quad \text{mi-}$$

$$\boxed{t_{11} > t_{22}} \quad \text{max: } 2\varphi = \arctan \frac{t_{12}}{\frac{1}{2}(t_{11} - t_{22})} \Rightarrow \varphi_{\text{max}} = \frac{1}{2} \arctan \frac{2t_{12}}{t_{11} - t_{22}}$$

$$\text{mi- } \varphi_{\text{mi-}} = \frac{1}{2} \arctan \frac{2t_{12}}{t_{11} - t_{22}} + \frac{\pi}{2}$$

6

$$\boxed{t_{11} < t_{22}} \quad \text{max: } 2\varphi = \arctan \frac{2t_{12}}{t_{11} - t_{22}} + \pi = 0 \Rightarrow \varphi = \frac{1}{2} \arctan \frac{2t_{12}}{t_{11} - t_{22}} - \frac{\pi}{2}$$

$$\text{min: } \varphi = \frac{1}{2} \text{dctg} \frac{2t_{12}}{t_{11} - t_{22}}$$

$$t_{-\vec{n}} = (-\vec{n}) \cdot \underline{t}(\vec{n}) = t_n$$

Največja normalna napetost je

$$\sigma_{\max} = \frac{1}{2} (t_x + t_y) + \sqrt{(t_x - t_y)^2 + 4t_{xy}^2} = \frac{1}{2} (\text{sl } \underline{t} + \sqrt{(\text{sl } \underline{t})^2 - 4 \det \underline{t}}),$$

najmanjša pa

$$\sigma_{\min} = \frac{1}{2} (t_x + t_y - \sqrt{(t_x - t_y)^2 + 4t_{xy}^2}) = \frac{1}{2} (\text{sl } \underline{t} - \sqrt{(\text{sl } \underline{t})^2 - 4 \det \underline{t}}).$$

$$t_x = t_{11}$$

$$t_y = t_{22}$$

$$t_{xy} = t_{12}$$

$$\begin{aligned} (\text{sl } \underline{t})^2 - 4 \det \underline{t} &= (t_{11} + t_{22})^2 - 4(t_{11}t_{22} - t_{12}^2) = \\ &= t_{11}^2 + t_{22}^2 + 2t_{11}t_{22} - 4t_{11}t_{22} + 4t_{12}^2 \end{aligned}$$

$$\underbrace{\quad - 2t_{11}t_{22} \quad}_{(t_{11} - t_{22})^2} = \underline{(t_{11} - t_{22})^2 + 4t_{12}^2}$$

Smerem v katerih ima neposredni tenzor elastičnosti največjo napetost pravimo glavne smeri.

Glavni smeri sta med seboj pravokotni.

Smeri ekstremalne normalne napetosti sta

$$\varphi_{\sigma}^1 = \frac{1}{2} \arctan \frac{2t_{xy}}{t_x - t_y}, \quad \varphi_{\sigma}^2 = \varphi_{\sigma}^1 + \frac{\pi}{2}.$$

$$\varphi_{\max} = \frac{1}{2} \arctan \frac{2t_{12}}{t_{11} - t_{22}} + \begin{cases} 0 & t_{11} \geq t_{22} \\ \pi/2 & t_{11} < t_{22} \end{cases},$$

minimalna pa je

$$\varphi_{\min} = \varphi_{\max} + \frac{\pi}{2}.$$

Smeri največje in najmanjše normalne napetosti oklepata pravi kot.

Ekstremalnim normalnim napetostim pravimo tudi glavne napetosti, njunima smerema pa glavne smeri.

$$k_n = \text{tg } \delta = \frac{2t_{12}}{t_{11} - t_{22}}$$

$$k_n \cdot k_s = -1$$

Določitev smeri ekstremalne strižne napetosti

$$t_{12}' = -\frac{1}{2}(t_{11} - t_{22}) \sin 2\varphi + t_{12} \cos 2\varphi = C \cos(2\varphi - \delta)$$

$$C = \sqrt{\frac{1}{4}(t_{11} - t_{22})^2 + t_{12}^2}$$

$$C \cos 2\varphi \cos \delta + C \sin 2\varphi \sin \delta$$

$$k_s = \text{tg } \delta = \frac{-\frac{1}{2}(t_{11} - t_{22})}{t_{12}} = -\frac{t_{11} - t_{22}}{2t_{12}}$$

$$\begin{cases} t_{12} = C \cos \delta \\ -\frac{1}{2}(t_{11} - t_{22}) = C \sin \delta \end{cases}$$

$$\sigma_{\max} = \frac{1}{2}(t_{11} + t_{22}) + \sqrt{\frac{1}{4}(t_{11} - t_{22})^2 + t_{12}^2}$$

$$\sigma_{\min} = \frac{1}{2}(t_{11} + t_{22}) - \sqrt{\frac{1}{4}(t_{11} - t_{22})^2 + t_{12}^2}$$

$$\frac{1}{2}(\sigma_{\max} - \sigma_{\min}) = \sigma_{\max}$$

Ekstremalna strižna napetost je

$$\tau_{\text{ext}} = \pm \frac{1}{2}(\sigma_{\max} - \sigma_{\min})$$

V koordinatnem sistemu z osema v smereh ekstremalnih normalnih napetosti je strižna komponenta

$$\tau_{\text{ext}} = -\frac{1}{2} \arctg \frac{t_{11} - t_{22}}{2t_{12}} \left(+ \frac{\pi}{2} \right)$$

nenta pripadajoče matrike napetostnega tenzorja enaka nič.

Pripadajoča smer ekstremalne strižne napetosti oklepa kot $\pi/4$ s smerjo ekstremalne normalne napetosti.

v ext. smeri
normalna nap.

$$\begin{aligned} t_{12}' &= -\frac{1}{2}(t_{11} - t_{22}) \sin 2\varphi + t_{12} \cos 2\varphi = \\ &= \cos 2\varphi \left(-\frac{1}{2}(t_{11} - t_{22}) \text{tg } 2\varphi + t_{12} \right) \end{aligned}$$

$$\text{tg } 2\varphi = \frac{2t_{12}}{t_{11} - t_{22}}$$

Mohrove krožnice osnovnih napetostnih stanj

